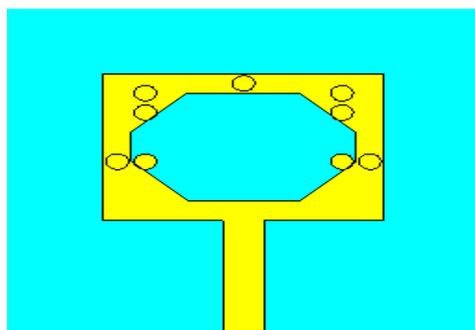
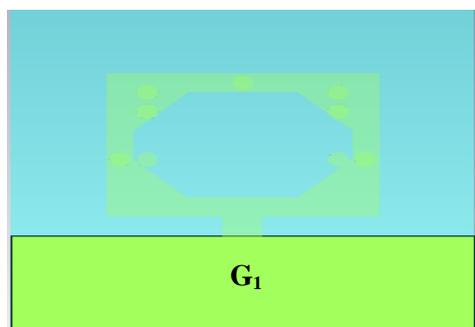


(d) Bottom View #3 (three ground strips: 3PG)

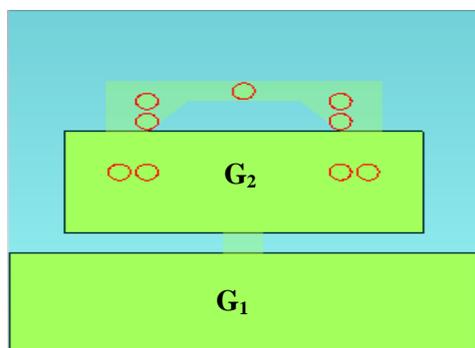
Fig. 1. Proposed filtenna #1 with different ground structures



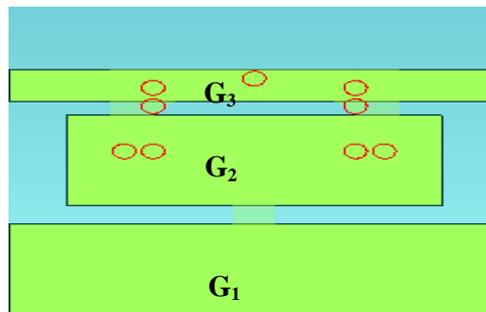
(a) Top view of proposed patch filtenna #2



(b) Bottom View #1 (partial ground: 1PG)



(c) Bottom View #2 (two ground strips: 2PG)



(d) Bottom View #3 (three ground strips: 3PG)

Fig. 2. Proposed filtenna #2 with different ground structures

TABLE I  
Vias dimensions and positions of filtenna #1

No.	Position (x, y)	Radius	Height
1	(8, 21)	0.5	1.67
2	(8, 26)	0.5	1.67
3	(12, 24)	0.5	1.67
4	(16, 26)	0.5	1.67
5	(21, 24.5)	0.5	1.67
6	(24, 26)	0.5	1.67
7	(26, 21)	0.5	1.67

TABLE II  
Vias dimensions and positions of filtenna #2

No.	Position (x, y)	Radius	Height
1	(8, 18)	0.8	1.67
2	(10, 18)	0.8	1.67
3	(10, 23)	0.8	1.67
4	(10, 25)	0.8	1.67
5	(17, 26)	0.8	1.67
6	(24, 25)	0.8	1.67
7	(24, 23)	0.8	1.67
8	(24, 18)	0.8	1.67
9	(26, 18)	0.8	1.67

## II. SIMULATION RESULTS

The two filtenna configurations discussed in the previous section are simulated using microwave CST\_Studio, and the results are presented in this section. Table (3), summaries all considered cases of our simulations. First, effects of adding slot and/or short circuit vias on the patch resonance are evaluated

and investigated as compared to the conventional patch “CP “ (rectangular patch with the same dimensions and has no slot nor vies and it has full ground). The results are presented in Fig.3 and Fig.4. It is clear from these figures that the conventional patch has multi resonance frequencies due to the mismatch between the patch and the feed line (Inset has not been used). In addition, adding either slot or vies has the effect of shifting the resonance frequency bands.

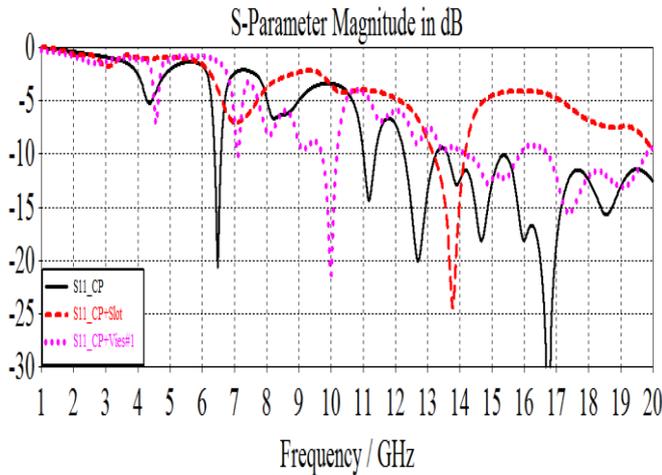


Fig. 3.  $|S_{11}|$  of CP versus adding slot or short circuit vies#1

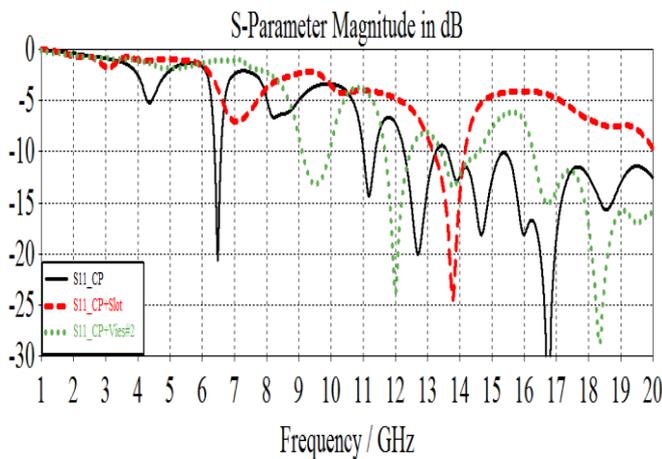


Fig. 4.  $|S_{11}|$  of CP versus adding slot or short circuit vies#2

Moreover, the effects of combining both slot and short circuit vies are presented in Fig.5. It is clear from the figure that, the resonance frequencies as well as the frequency bands is dependent on the slot size and the vies geometry. The first vies distribution (Vies#1: given in table (1)) has the narrow resonances at 4.0 and 8.5 GHz and wideband resonance at 13.7 GHz. On the other hand, a single wideband resonance has been occurred in case of second vies distribution (vies#2: given in table (2)). Second, the effects of partial ground (single ground strip) in presence of slot and vies has been investigated and the results are illustrated in Fig.6 and Fig.7. The effect of adding slot and vies along with the partial ground act as a bandpass filter built-in with conventional patch antenna. This leads to compact dual broadband antenna (1<sup>st</sup> band from 3.0 GHz to 5.0 GHz, and 2<sup>nd</sup> band from 12.0 GHz to 15.5 GHz).

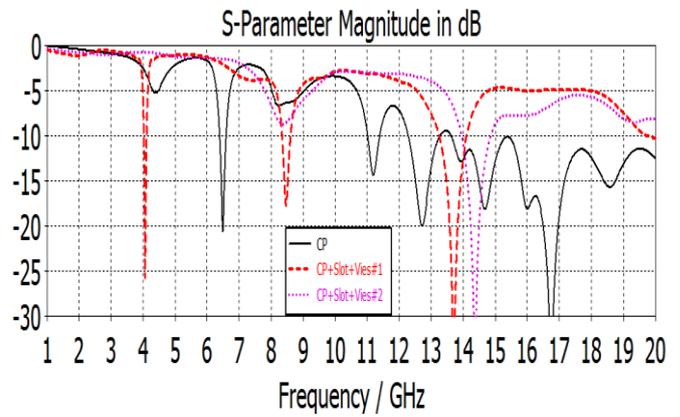


Fig. 5.  $|S_{11}|$  of CP versus adding slot and short circuit vies

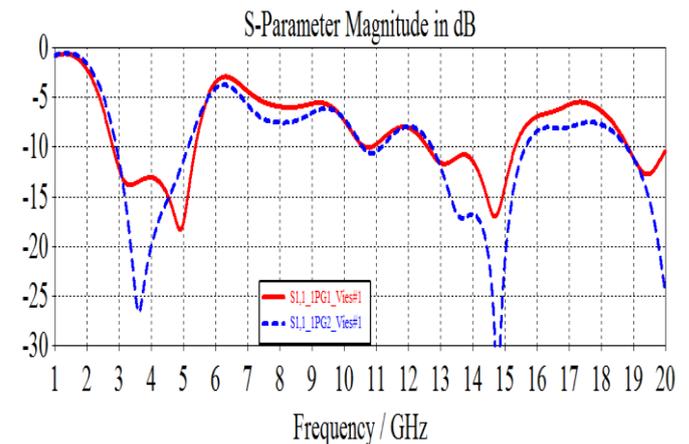


Fig. 6.  $|S_{11}|$  of Proposed filtennas (adding slot and vies) with partial ground of length 10.0 mm

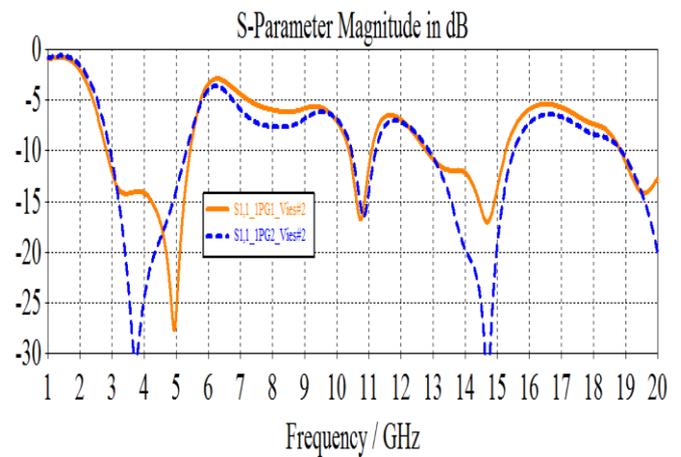


Fig. 7.  $|S_{11}|$  of Proposed filtennas (adding slot and vies) with partial ground of length 11.0 mm

The third study is to investigate the effect of two ground strips in presence of slot and different via distributions on patch resonances. A parametric study has been performed for the dimensions of the two ground strips and vies listed in table (1) through table (3). The results of simulation are presented in Fig.8 and Fig.9. It is clear from these figures that the conventional patch with two ground strips and short circuit vies

can operate at different isolated frequency bands. Thus, the antenna resonances and bandwidths can be easily controlled. In fact, the obtained results indicate very important issue for filtenna design. An arbitrary conducting patch (may have a slot) mounted on substrate of partitioned ground strips with arbitrary geometries in presence of short circuit vies act as bandpass filter. The characteristic of such filter depends on three main parameters. This includes the number of vies and their geometries, ground geometry, and slot size. In addition, the proposed filtennas are very compact in size, and it can operate in a wideband from 3.0 GHz to 4.5 GHz as shown form these figures. Finally, the fourth study is to investigate the effect of three ground strips in presence of slot and different via distributions on the patch resonances. The results of simulation are illustrated in Fig.10 and Fig.11. As it is clear for these figures, the proposed filtenna can operate at different isolated broadband and ultra-wideband frequencies. For example, the proposed filtenna#2 can resonate in an ultra-wideband from 12.0 GHz to 15.5 GHz while it can also resonate in a wideband from 2.5 GHz to 3.5 GHz (see Fig. 11, black curve-solid).

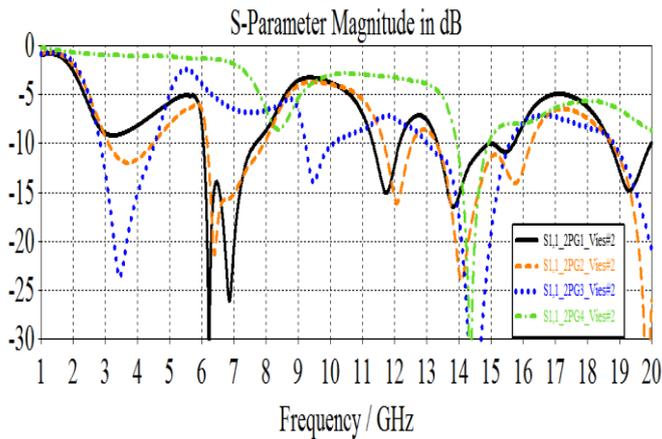


Fig. 8.  $|s_{11}|$  of proposed filtenna #1(2PG)

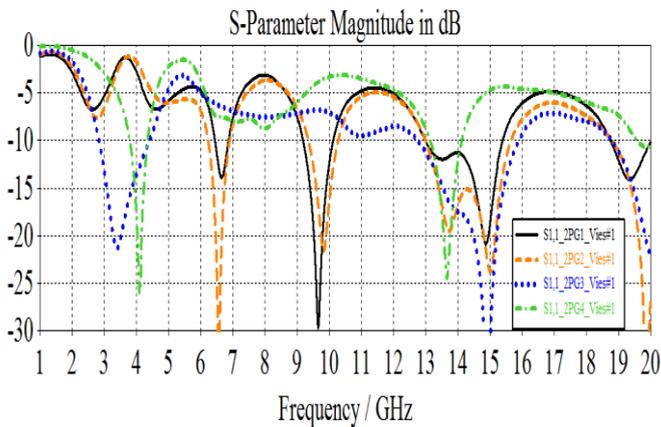
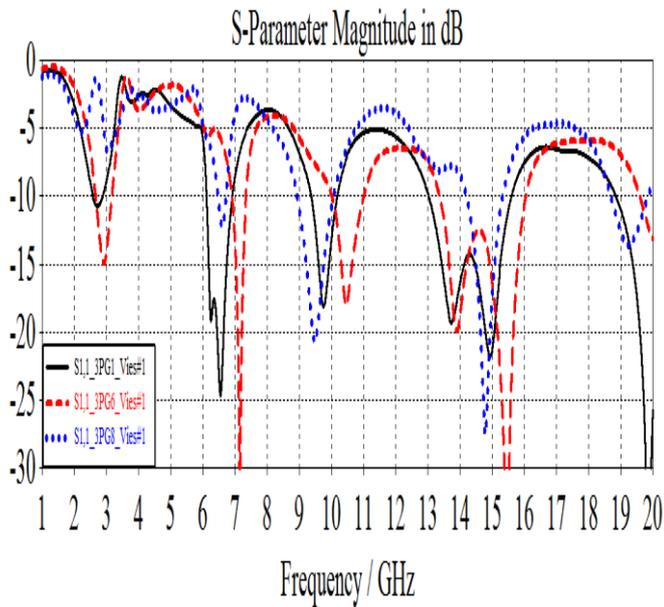
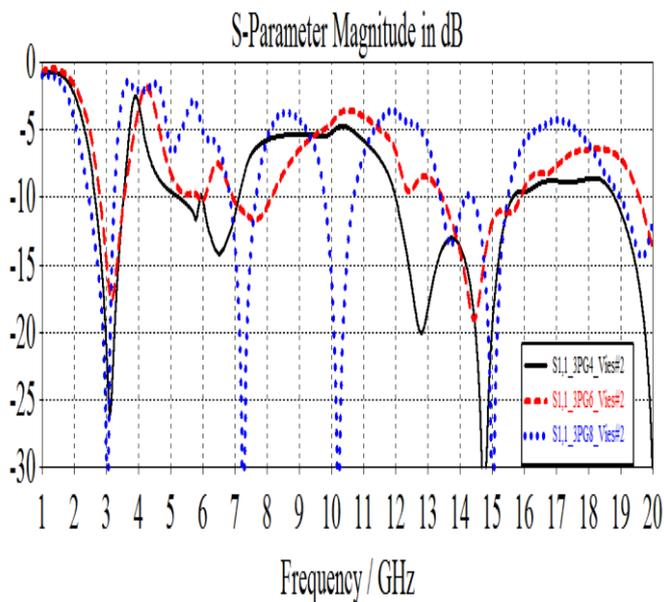


Fig. 9.  $|s_{11}|$  of Proposed filtenna #2(2PG)

TABLE III  
Dimensions and locations of partitioned ground

Length and Width of each ground Strip ( $W_n, L_n$ )	$G_1$	$G_2$	$G_3$	Case #
	(0, 34)	----	----	S11_CP+ Vies#1
	(0,34)	----	----	S11_CP+ Vies#2 S11_CP
	(0, 34)	----	----	<b>S11-1PG1</b>
	(0,10)	----	----	
	(0, 34)	----	----	<b>S11-1PG2</b>
	(0,11)	----	----	
	(0, 34)	(0, 34)	----	<b>S11-2PG1</b>
	(0,10)	(15,27)	----	
	(0, 34)	(0, 34)	----	<b>S11-2PG2</b>
	(0,11)	(15,27)	----	
	(0, 34)	(7, 27)	----	<b>S11-2PG3</b>
	(0,11)	(20, 27)	----	
	(0, 34)	(7, 27)	----	<b>S11-2PG4</b>
	(0,19)	(20, 27)	----	
	(0, 34)	(0, 34)	(0, 34)	S11-3PG1
	(0,11)	(15,21.5)	(23.5, 30)	
	<b>(0, 34)</b>	<b>(0, 34)</b>	<b>(0, 34)</b>	<b>S11-3PG2</b>
	<b>(0, 11)</b>	<b>(15,21.5)</b>	<b>(23.5, 27)</b>	
	(0, 34)	(0,34)	(0, 34)	S11-3PG3
(0,11)	(15,21.5)	(23.5, 34)		
(0, 34)	(0, 34)	(0, 34)	S11-3PG4	
(0,11)	(18,21.5)	(23.5, 27)		
<b>(0, 34)</b>	<b>(0, 34)</b>	<b>(0, 34)</b>	<b>S11-3PG5</b>	
<b>(0,12)</b>	<b>(15,21.5)</b>	<b>(23.5, 27)</b>		
(0, 34)	(4, 30)	(0, 34)	S11-3PG6	
(0,12)	(15,21.5)	(23.5, 27)		
<b>(0, 34)</b>	<b>(4, 30)</b>	<b>(7, 27)</b>	<b>S11-3PG7</b>	
<b>(0,12)</b>	<b>(15,21.5)</b>	<b>(23.5, 27)</b>		
<b>(0, 34)</b>	<b>(0, 34)</b>	<b>(0, 34)</b>	<b>S11-3PG8</b>	
<b>(0,10)</b>	<b>(13, 21)</b>	<b>(22, 34)</b>		

Fig. 10.  $|S_{11}|$  of proposed filtena #1 (3PG)Fig. 11.  $|S_{11}|$  of proposed filtena #2 (3PG)

#### IV. CONCLUSION

New compact patch filtenna structures have been proposed, analyzed, designed and simulated (narrowband, broadband, dual-band, and ultra-wideband). The results of simulation show that the resonance frequencies of our proposed compact patch filtenna structures can be controlled within different isolated bands. To design such filtenna, three steps are required. First, select a conventional patch antenna to resonate at a specific required frequency in the 3G/4G wireless band. Second, the add slot and array of vies to the patch antenna. Finally, the ground plane is divided into two or three partitions. These steps

have been verified using two different vies geometries and three different ground shapes for the same patch. Based on our results, the partitioned ground, slot and short circuit vies act as built-in bandpass filter with conventional patch antenna. The proposed filtenna structures can be used for many of applications. This includes mobile, GPS, wireless networks, and radar systems. The present paper has a new and simple method to design a planar filtenna and/or operates at the desired frequency bands. Future work will include design and implementation of two port filtenna for MIMO applications using our proposed method.

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