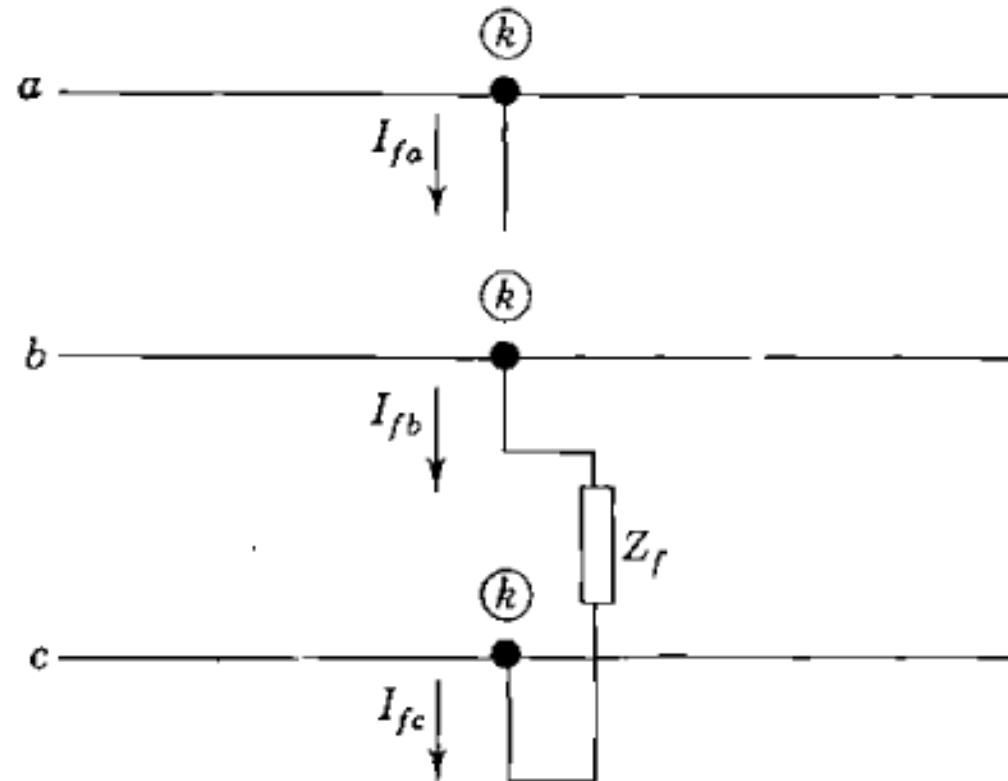


Line-Line Fault



$$I_{fa} = 0 \quad I_{fb} = -I_{fc} \quad V_{kb} - V_{kc} = I_{fb} Z_f$$

Since $I_{fb} = -I_{fc}$ and $I_{fa} = 0$, the symmetrical components of current are

$$\begin{bmatrix} I_{fa}^{(0)} \\ I_{fa}^{(1)} \\ I_{fa}^{(2)} \end{bmatrix} = \frac{1}{3} \begin{bmatrix} 1 & 1 & 1 \\ 1 & a & a^2 \\ 1 & a^2 & a \end{bmatrix} \begin{bmatrix} 0 \\ I_{fb} \\ -I_{fb} \end{bmatrix}$$

and multiplying through in this equation shows that

$$I_{fa}^{(0)} = 0$$

$$I_{fa}^{(1)} = -I_{fa}^{(2)}$$

$$\begin{aligned}
 V_{kb} - V_{kc} &= (V_{kb}^{(1)} + V_{kb}^{(2)}) - (V_{kc}^{(1)} + V_{kc}^{(2)}) = (V_{kb}^{(1)} - V_{kc}^{(1)}) + (V_{kb}^{(2)} - V_{kc}^{(2)}) \\
 &= (a^2 - a)V_{ka}^{(1)} + (a - a^2)V_{ka}^{(2)} = (a^2 - a)(V_{ka}^{(1)} - V_{ka}^{(2)})
 \end{aligned}$$

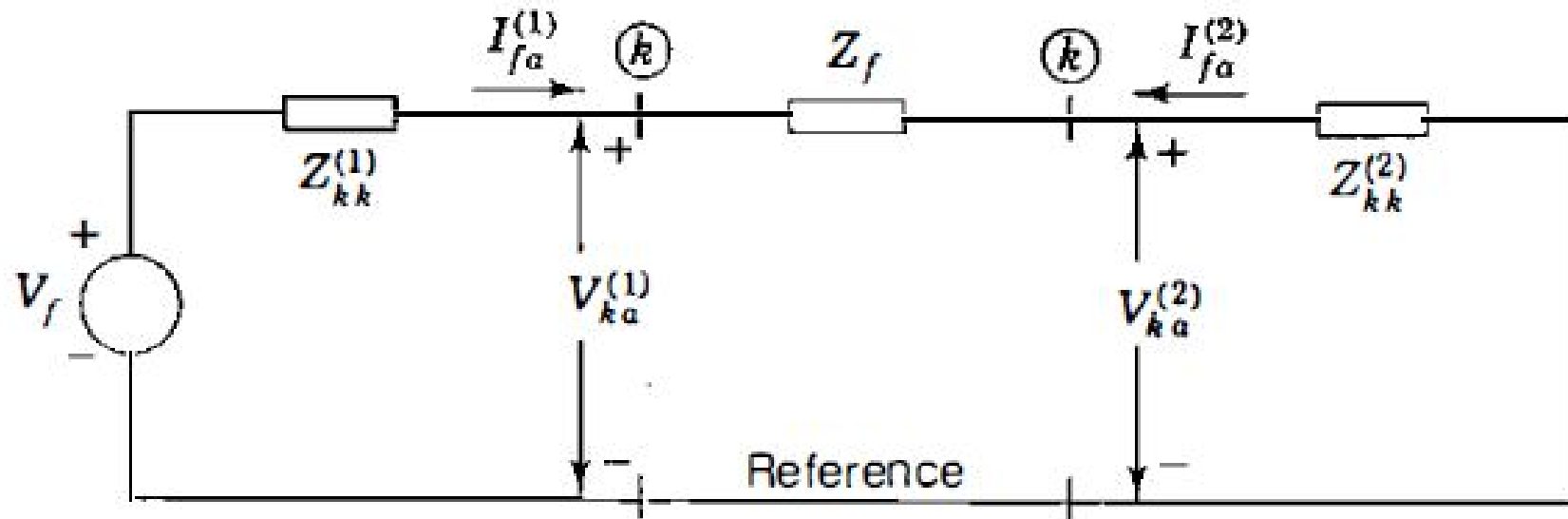
$$I_{fb}Z_f = (I_{fb}^{(1)} + I_{fb}^{(2)})Z_f = (a^2I_{fa}^{(1)} + aI_{fa}^{(2)})Z_f$$

Equating both terms and setting $I_{fa}^{(2)} = -I_{fa}^{(1)}$

$$(a^2 - a)(V_{ka}^{(1)} - V_{ka}^{(2)}) = (a^2 - a)I_{fa}^{(1)}Z_f$$

OR

$$V_{ka}^{(1)} - V_{ka}^{(2)} = I_{fa}^{(1)}Z_f$$



$$I_{fa}^{(1)} = -I_{fa}^{(2)} = \frac{V_f}{Z_{kk}^{(1)} + Z_{kk}^{(2)} + Z_f}$$

$$I_{fa}^{(1)} = -I_{fa}^{(2)} = \frac{V_f}{Z_{kk}^{(1)} + Z_{kk}^{(2)} + Z_f}$$

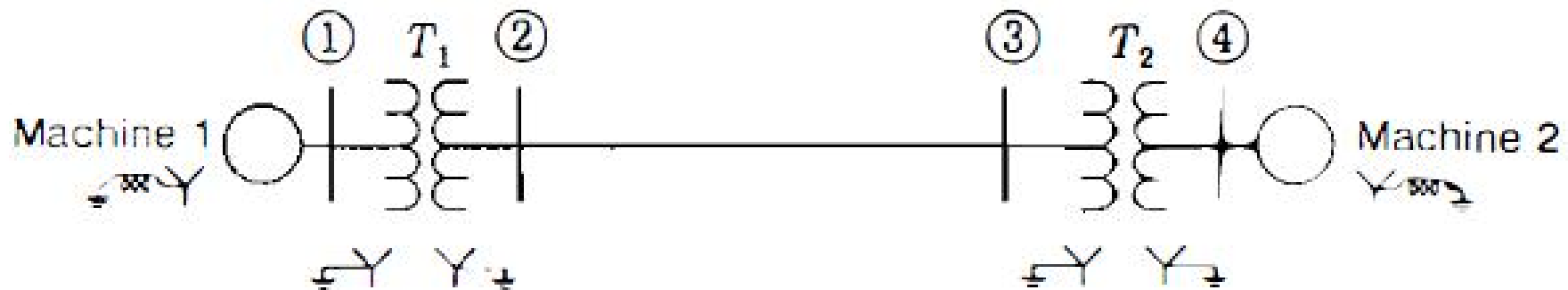
Example 12.3. The same system as in Example 12.1 is operating at nominal system voltage without prefault currents when a bolted line-to-line fault occurs at bus ③. Using the bus impedance matrices of the sequence networks for subtransient conditions, determine the currents in the fault, the line-to-line voltages at the fault bus, and the line-to-line voltages at Bus bar 2

Example 12.1. Two synchronous machines are connected through three-phase transformers to the transmission line shown in Fig. 12.5. The ratings and reactances of the machines and transformers are

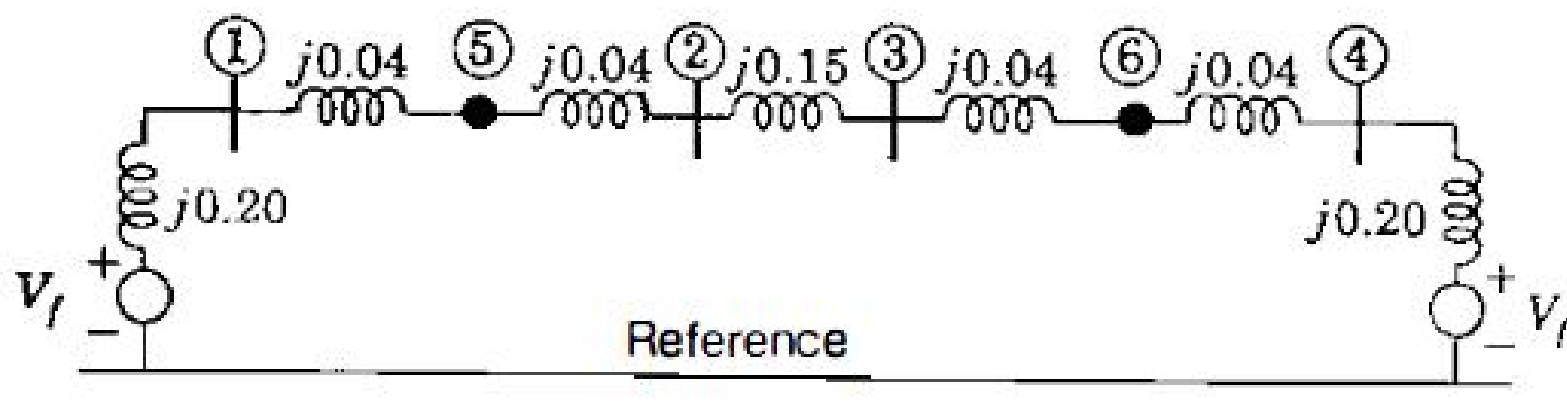
Machines 1 and 2: 100 MVA, 20 kV; $X''_d = X_1 = X_2 = 20\%$,

$X_0 = 4\%$, $X_n = 5\%$

Transformers T_1 and T_2 : 100 MVA, 20/345 kV ; $X = 8\%$

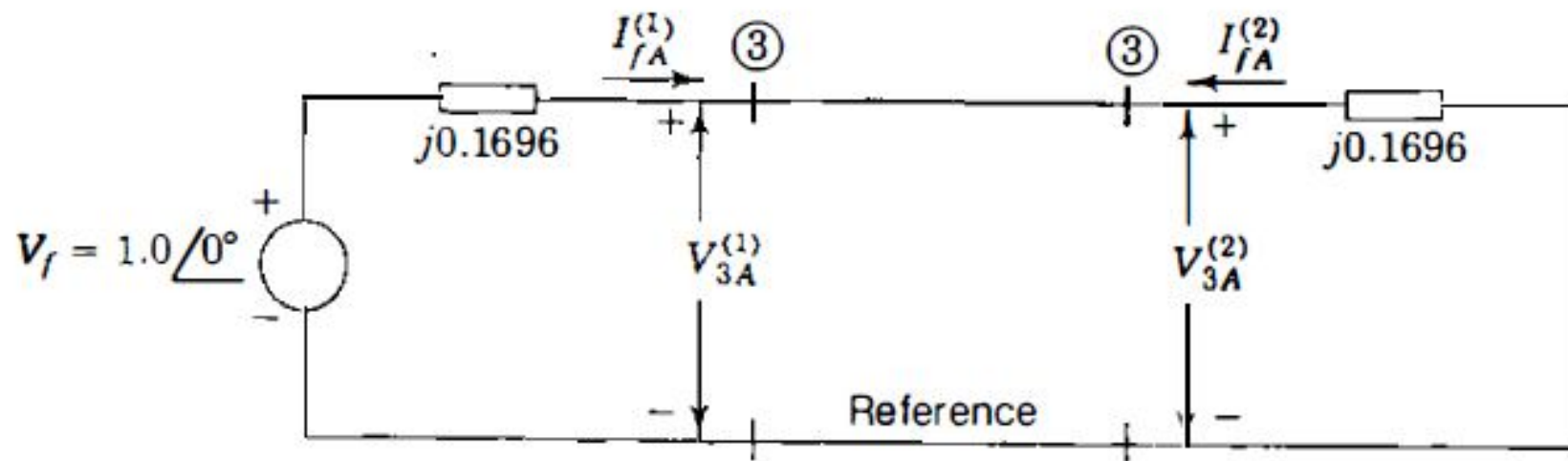


Both transformers are solidly grounded on two sides. On a chosen base of 100 MVA, 345 kV in the transmission-line circuit the line reactances are $X_1 = X_2 = 15\%$ and $X_0 = 50\%$. The system is operating at nominal voltage without pre-fault



Positive Sequence Network

$$Z(\text{positive sequence}) = Z(\text{negative sequence}) = j0.1696 \text{ p.u.}$$



$$I_{fA}^{(1)} = -I_{fA}^{(2)} = \frac{V_f}{Z_{33}^{(1)} + Z_{33}^{(2)}} = \frac{1 + j0}{j0.1696 + j0.1696} = -j2.9481 \text{ per unit}$$

Since $I_{fA}^{(0)} = 0$, the components of currents in the fault are calculated from

$$I_{fA} = I_{fA}^{(1)} + I_{fA}^{(2)} = -j2.9481 + j2.9481 = 0$$

$$\begin{aligned} I_{fB} &= a^2 I_{fA}^{(1)} + a I_{fA}^{(2)} = -j2.9481(-0.5 - j0.866) + j2.9481(-0.5 + j0.866) \\ &= -5.1061 + j0 \text{ per unit} \end{aligned}$$

$$I_{fC} = -I_{fB} = 5.1061 + j0 \text{ per unit}$$

Current In kA

$$I_{fA} = 0$$

$$I_{fB} = -5.1061 \times 167.35 = 855 \angle 180^\circ \text{ A}$$

$$I_{fC} = 5.1061 \times 167.35 = 855 \angle 0^\circ \text{ A}$$

$$V_{3A}^{(0)} = 0$$

$$V_{3A}^{(1)} = V_{3A}^{(2)} = 1 - Z_{kk}^{(1)} I_{fA}^{(1)} = 1 - (j0.1696)(-j2.9481) = 0.5 + j0 \text{ per unit}$$

Line-to-ground voltages at fault bus (3) are

$$V_{3A} = V_{3A}^{(0)} + V_{3A}^{(1)} + V_{3A}^{(2)} = 0 + 0.5 + 0.5 = 1.0 \angle 0^\circ \text{ per unit}$$

$$V_{3B} = V_{3A}^{(0)} + a^2 V_{3A}^{(1)} + a V_{3A}^{(2)} = 0 + a^2 0.5 + a 0.5 = 0.5 \angle 180^\circ \text{ per unit}$$

$$V_{3C} = V_{3B} = 0.5 \angle 180^\circ \text{ per unit}$$

Line-to-line voltages at fault bus ③ are

$$V_{3, AB} = V_{3A} - V_{3B} = (1.0 + j0) - (-0.50 + j0) = 1.5 \angle 0^\circ \text{ per unit}$$

$$V_{3, BC} = V_{3B} - V_{3C} = (-0.5 + j0) - (-0.50 + j0) = 0$$

$$V_{3, CA} = V_{3C} - V_{3A} = (-0.5 + j0) - (1.0 + j0) = 1.5 \angle 180^\circ \text{ per unit}$$

For calculation of voltage at Bus Bar 2

$$I_{f2-3}^{(1)} = \frac{(-j2.95) * (j0.28)}{j0.28 + j0.43}$$

$$I_{f2-3}^{(1)} = -j1.1634 \text{ p.u.}$$

$$I_{f2-3}^{(2)} = j1.1634 \text{ p.u.}$$

$$V_{2a}^{(1)} = 1 - [(-j1.1643)(j0.28)] = 0.6742 \text{ p.u.}$$

$$V_{2a}^{(2)} = -(j1.1634)(j0.28) = 0.3258 \text{ p.u.}$$

$$V_{2a} = 1 \text{ p.u.}$$

$$V_{2b} = 0.584 \angle -150^\circ \text{ p.u.}$$

$$V_{2c} = 0.584 \angle 150^\circ \text{ p.u.}$$

$$V_{2ab} = V_{2a} - V_{2b}$$

$$V_{2bc} = V_{2b} - V_{2c}$$

$$V_{2ca} = V_{2c} - V_{2a}$$